

### **Review Article**

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Received: August 5, 2019 Revised: September 27, 2019 Accepted: September 27, 2019

See commentary "Biomaterials in Spinal Implants: A Review" via https://doi. org/10.14245/ns.2040126.063.



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### Biomaterials in Spinal Implants: A Review

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The aim to find the perfect biomaterial for spinal implant has been the focus of spinal research since the 1800s. Spinal surgery and the devices used therein have undergone a constant evolution in order to meet the needs of surgeons who have continued to further understand the biomechanical principles of spinal stability and have improved as new technologies and materials are available for production use. The perfect biomaterial would be one that is biologically inert/compatible, has a Young's modulus similar to that of the bone where it is implanted, high tensile strength, stiffness, fatigue strength, and low artifacts on imaging. Today, the materials that have been most commonly used include stainless steel, titanium, cobalt chrome, nitinol (a nickel titanium alloy), tantalum, and polyetheretherketone in rods, screws, cages, and plates. Current advancements such as 3-dimensional printing, the ProDisc-L and ProDisc-C, the ApiFix, and the Mobi-C which all aim to improve range of motion, reduce pain, and improve patient satisfaction. Spine surgeons should remain vigilant regarding the current literature and technological advancements in spinal materials and procedures. The progression of spinal implant materials for cages, rods, screws, and plates with advantages and disadvantages for each material will be discussed.

Keywords: Spine, Surgery, Biomaterials, Rods, Screws, Cages

#### INTRODUCTION

Spinal surgery has existed for since Jules Gerin first attempted surgical scoliosis correction in 1839. In the late 1800's Dr. Berthold Earnest Hadra created a fixation device for C6–7 dislocations using silver wire that he later applied to the treatment of Potts disease. His methods gained the attention of orthopedists across Europe who modified it to stabilize the spinous processes, laminae, and pedicles for the cervical spine using wiring, lateral mass screws, plates, and rods, and pedicle screws. Since its inception, spinal surgery and the devices used therein have undergone a constant evolution in order to (1) meet the needs of surgeons who have continued to further understand the biomechanical principles of spinal stability and (2) have improved as new technologies and materials are available for production

use. Spinal implants need to demonstrate biostability (ability to resist the effects of micro-oganisms) and biocompatibility (not harmful to living tissue) and the difficulty in finding an optimal material lies in determining a material with an appropriate Young's modulus (also known as Elastic Modulus, the stress to strain ratio which demonstrates increased stiffness and brittleness with higher values), stiffness, and fatigue. The materials that have been most commonly used include stainless steel (SS), titanium, cobalt chrome, nitinol (a nickel titanium alloy), tantalum, and polyetheretherketone (PEEK). The perfect biomaterial would be one that is biologically inert/compatible, has a Young's modulus similar to that of the bone where it is implanted, high tensile strength, stiffness, fatigue strength, and low artifacts on imaging. This review article will discuss the uses of these various biomaterials and their application in spinal implants. The

progression of spinal implant materials for cages, rods, screws, and plates will be discussed with advantages and disadvantages for each material as have been demonstrated in multiple clinical studies.

# BIOMATERIALS IN VARIOUS TYPES OF SPINAL IMPLANTS

#### 1. Cages

Cages are spinal implants that act as a stabilizer for force distribution between vertebral bodies and to restore the height of the intervertebral and foramina space.<sup>7</sup> They provide a graft for vertebrae to refuse and heal when an intervertebral disc has failed.<sup>7</sup> Originally, autologous bone grafts were used; however, donor site morbidity combined with high failure rates resulting from collapse, subsidence, retropulsion, or resorption of the graft with prolonged healing time was frequently seen.<sup>8</sup>

Cages are typically made of metal – ranging from pure titanium (PTi), titanium composite/alloy, ceramic – usually silicon nitride, or plastic – usually PEEK or another bioinert plastic such as acrylic by itself or coated in another material (such as hydroxyapatite [HA] or titanium).<sup>9-14</sup> These cages are porous as to allow the bones to grow through them and stabilize.<sup>15</sup>

The most popular materials used today are titanium (titanium-aluminum-vanadium, Ti6Al4V) and PEEK (Tables 1, 2). <sup>16</sup> PTi and titanium alloys are the preferred metal in orthopaedic implants due to their high fracture resistance and biocompatibility. <sup>17</sup> Titanium has a superior biocompatibility, corrosion re-

sistance, and Young's modulus compared with SS and cobalt counterparts (Fig. 1). The major issue with polished or abraded titanium is its lack of bone-bonding ability, hence increased research has been done to coat/dope titanium alloys to improve bone-bonding.

PEEK has a similar Young's modulus compared to bone, without sufficient doping such as titanium plasma spray and vapor deposition, has weak surface interfaces that can fracture upon cage implantation.<sup>19</sup> PEEK has radiographic properties that allow surgeons to monitor possible migration and success of the

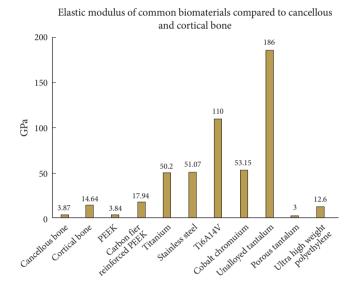


Fig. 1. Young's modulus of common biomaterials.

Table 1. Common biomaterials used in spine surgery

Implant	Implementation procedure	Standard materials	Upcoming materials
Cage	Anterior/posterior interbody fusion - Restores height of collapsed disc from injury, DDD, or scoliosis.	Titanium PEEK Ceramic Acrylic	Bioactive glass Silicon nitride Apatite-Wollastonite poly(ε-caprolactone)+HA (biodegradable)
Screws	<u>Pedicle screw fixation</u> - Holds vertebrae together to attach plates and rods.	Titanium (Ti6Al4V) doped with: HA CaP ECM Tantalum	Carbonated apatite
Rods	<u>Spinal fusion</u> - Adds stability to a spinal implant. Used for scoliosis correctional surgery.	Titanium CoCr PEEK Stainless steel Nitinol	Ti-Mo Oxygen-modified beta-type Ti-Cr Biodegradable materials
Plates	Spinal stabilization	Titanium	Biodegradable materials

DDD, degenerative ddisc disease; PEEK, polyetheretherketone; Ti6Al4V, titanium-aluminum-vanadium; HA, hydroxyapatite; CaP, calcium phosphate; ECM, extracellular matrix; CoCr, cobalt-chromium alloys; Ti-Mo, titanium-molybdenum; Ti-Cr, titanium-chronium.

implant. However, the primary issue with PEEK is that it is hydrophobic and unable to bond to bone to achieve a solid fusion. <sup>20</sup> Research has shown that there may be associations with cage migration and pseudarthrosis. <sup>21</sup> It has also been shown that PEEK has a significantly lower stress compression strength compared to titanium (2.5 times weaker). <sup>22</sup> However, for anterior cervical discectomy and fusion (ACDF) surgeries, it has been shown that PEEK cages have a significantly lower loss of Cobb angles and lower cage subsidence rate compared to titanium (34.5% and 5.4% respectively). <sup>23</sup>

Increased research for advancements in disc separation has been made to find more biocompatible materials than titanium and PEEK to improve bone grafting. Experimentation with silicon nitride ( $Si_3N_4$ ) showed no significant different compared to PEEK.<sup>24</sup> Other studies have tried an Apatite-Wollastonite (A/W) ceramic cage to replace the PEEK cages. However, like the silicon nitride cage materials, there was no significant advantage of the A/W cage compared to the porous PEEK cages.<sup>25</sup> An

additional study performed stress/strain tests on porous biodegradable materials such as poly( $\epsilon$ -caprolactone) combined with HA. Computational and *in vitro* modeling confirmed the mechanical integrity of the new biodegradable material within the human spine. <sup>26</sup> Many of these studies have demonstrated that there are many theoretical models that seem to have promising results; however, no clinical data have been published in human trails to date for these materials.

#### 2. Rods

Spinal rods are used in conjunction with other spinal implants to add stability to spinal implant structure. Rods are contoured to a specific patient to fit the spine. In 1962, Dr. Harrington introduced the "Harrington Rod" – an SS rod – for surgical treatment of scoliosis.<sup>27</sup> However, rod contouring (such as French Benders) imparts marks and weaknesses onto the rod that compromise its durability.<sup>28</sup>

Rods were initially made of SS to provide sufficient stability

Table 2. Characteristics of biomaterials

Materials	Advantages	Disadvantages	Application
Stainless steel	Very strong Very stiff Easily doped/alloyed to be stronger Inexpensive	Corrosion Relatively poor biocompatibility High artifacts in imaging	Scoliosis correction (rods) Formerly used in screws; now mostly replaced by titanium
Titanium	Lightweight Strong Flexible Biocompatible Easily doped/alloyed to be stronger	Relatively Expensive Some artifacts during imaging	Screws Rods Plates Cages
PEEK	Lightweight Flexible Relatively Inexpensive Biocompatible Easily doped/coated for improved grafting Low artifacts on imaging	Low Young's modulus Some grafting issues, but improved with coatings	Rods Cages Disc replacement
CoCr	Strong Flexible Biocompatible	Relatively expensive High artifacts on imaging	Adolescent scoliosis correction (rods) to provide a more flexible buttress for the spine to curve about.
Ceramic	Relatively inexpensive Biocompatible Ware resistant Easily doped	Brittle Grafting issues, but can be improved with coating/doping	Used in cage biomaterials Doped with A/W
Nitinol	Strong "Memory metal" (shape recovery)	Relatively expensive Sometimes not stiff enough for proper correction	Not frequently used, but can be implemented for young scoliosis correctional surgery.
Tantalum	High frictional characteristics Low Young's modulus	Very expensive Not stuff enough for some spinal corrections.	Not frequently used due to its price. Has primarily been phased out completely by titanium.

PEEK, polyetheretherketone; CoCr, cobalt-chromium alloys; A/W, Apatite-Wollastonite.

and stiffness for proper spine alignment.<sup>29</sup> Today, rods are typically made of titanium or PEEK. The shift from SS to titanium resulted from titanium's improved biomechanical properties to bone (similar modulus elasticity of cortical bone), improved biocompatibility, and improvements in stress shielding of lumbar pedicle instrumentation.<sup>30,31</sup>

The metal rods used today fall into one of 3 alloy families: iron (Fe)-chromium (Cr)-nickel (Ni) alloys and austenitic SS, titanium and its alloys (PTi and Ti6Al4V alloy), and cobalt-chromium alloys (CoCr). These alloys were chosen because they are relatively biocompatible and are protected from corrosion by the presence of a stable oxide layer; however, SS is the least corrosion resistant.<sup>32</sup> Of these metals, titanium has gained popularity due to its biomechanical properties as well as its significantly few artifacts on imaging.<sup>33</sup>

These other metal rods are stiffer than titanium rods. CoCr rods have gained recent popularity with adolescent idiopathic scoliosis with promising frontal correction rate in all-screw constructs due to their increased rigidity compared to titanium, closer reflecting SS.  $^{34}$  CoCr provided fewer complications in human trials and allowed for better thoracic sagittal realignment compared to titanium (p = 0.01).  $^{35}$  The primary drawback of CoCr compared to titanium is cost and increased artifacts on MRI; however, a study has shown that the spinal canal and neural element analysis was not impinged by the CoCr artifacts.  $^{36}$ 

Nitinol (50% Ni and 50% Ti) rods—also called memory rods—are not as common as Ti since the metal is expensive and notch-sensitive.<sup>37</sup> Nitinol is unique compared to SS or Ti because it can be placed in the spinal canal with no inflammatory response from the lymph nodes or other organs.<sup>38</sup> Nitinol shape recovery force have been used to achieve scoliosis correction. However, Nitinol is not frequently used due to its higher costs and lower Young's modulus compared to Ti or SS rods.<sup>39</sup>

Besides the rigid metal rods, there are semirigid rods. One of the most popular is the PEEK rods. It has been shown that PEEK provides comparable stability compared to titanium rods of similar size. One advantages of PEEK compared to titanium are load sharing; PEEK rods allow for greater contact between the end plate and bone graft due to its improved biological compliance and elasticity. PEEK is a radiolucent material, providing an advantage over other metallic devices since it results in only minor artifact on postoperative computed tomography and magnetic resonance imaging; however, it is more difficult for clinicians to identify faults and breaks within the PEEK rods, thus some PEEK rods use a contrast agent to improve imaging. Some possible disadvantages to PEEK rods range from

higher failure rates with early reoperations and insufficient capabilities of PEEK to form a stable union with the screw interface, leading to increased rates of pseudarthrosis.<sup>42</sup>

Many biomechanical studies have shown that when rods are bent to fit a patient using a French bender, significant surface defects and weakness are introduced. And fatigue, fractures, and significant deformation almost always occur at these notch points and at the screw-rod junction. One study showed that notching and bending significantly reduces the mechanical stability of titanium alloy rods, but not SS rods (p < 0.05). Clinical studies have found that waved rods have significantly improved fusion rates compared to rigid pedicle screws (45/50 compared to 36/46, p = 0.039).

New research is being conducted to create more efficient and more failure-resistant materials. Beta-type titanium-molybdenum and oxygen-modified beta-type titanium-chronium alloys have demonstrated promising Young's Moduli, high bending strength, and high tensile strength. 44,46 A study has shown that polycarbonate-urethane rods demonstrated more comparable intradiscal pressure compared to titanium rods consistently through 3,000 loading cycles (p < 0.05).<sup>47</sup> Another study tested the feasibility of biodegradable rods for posterior lumbar fusions in vitro which demonstrated that the biodegradable rods—like the standard titanium rods—could withstand 5,000,000 dynamic compression cycles under a 145 N axial load. However, the biodegradable rods had a 20% and 80% decrease in Young's modulus after 6 months and 12 months. 48 Furthermore, both of these studies were done not done in human trials or under true biological conditions, thus not all the effects of wear and tear could be measured and tested.

#### 3. Pedicle Screws

Pedicle screws are frequently used in spinal surgeries. Pedicle screw and rod posterior spinal fusion has become the clinical standard for the treatment of scoliosis since the pedicle screws can redirect force through the powerful vertebral bodies.<sup>49</sup> To withstand such great force, pedicle screws need to be made of a material that is strong, but also bioinert, thus, many today are made of Ti6Al4V.<sup>50</sup>

While pedicle screws provide some of the best correctional results in spinal surgery, some of the most common complications of pedicle screw placement include loosening, pullout, and screw breakage that can severely affect the bone healing process.<sup>51</sup> Various studies have tried coating and doping the pedicle screws with different materials ranging from HA, calcium phosphate (CaP), polymethymethacrylate bone cement

(PMMA-BC), extracellular matrix (ECM), tantalum, and titanium plasma spray. It was found that coating the Ti6Al4V screws with HA can improve resistance against pullout force compared to uncoated  $(165.6 \pm 26.5 \text{N vs.} 103.1 \pm 30.2 \text{ N}, p < 0.001)^{52}$  and had an improved bone-to-implant contact  $(64\% \pm 31\% \text{ vs.} 9\% \pm 13\%)^{53}$  respectively.

A study that compared HA, CaP, and PMMA-BC showed that there was no significant difference between the controls versus HA or CaP ( $p_{HA} = 0.6$  and  $p_{CaP} = 0.234$ ); however, the pullout strength differences between PMMA-BC and control were significantly different (p = 0.026). 54 Although PMMC-BC has a significantly greater pullout strength compared to the control, it is a far more rigid and solidified cement structure and cannot be modified easily postoperationally compared to HA or CaP. Another study coated the Ti6Al4V pedicle screws with tantalum and analyzed numerous effects a thin tantalum coating had on the performance of the Ti6Al4V screws. The tantalum screws had improved bone osteoclast proliferation in vitro, strong integration capacity of trabecular bone surrounding the screws, and greater pullout strength 12 weeks after fixation compared to the conventional Ti6Al4V screws in vivo.55 Coating the pedicle screws with ECM also seemed to improve pullout strength when combined with HA compared to the uncoated screws. There was no significant difference in the pullout strength between the screws coated in just ECM vs screws just coated in HA, but there was a significant difference in pullout strength between screws coated in HA+ECM vs. HA or ECM alone.<sup>56</sup>

New developments in pedicle screws have not focused much on the Ti6Al4V screw itself, but rather novel coatings and/or new cement on the Ti6Al4V screw to improve fixation and pull-out strength. Lotz et al.  $^{57}$  performed cadaveric lumbar tests with uncoated pedicle screws and pedicle screws in conjunction with the carbonated apatite cancellous bone cement demonstrated an average 68% (p < 0.001) greater pullout strength compared to the control screws.

In addition to pedicle screw biomaterial properties, technological advancements in screw design have recently occurred. The first pedicle screws were monoaxial and although provided good vertebral stabilization and correction, had difficulty adequately seating the rod in the screw.<sup>58</sup> This deficiency could result in movement of the screw within the vertebral body—causing loosening of the screw—and/or inadequate closure of the screw-rod connection.<sup>59</sup> Polyaxial pedicle screws used in unilateral or bilateral fixation are made out of titanium.<sup>60</sup> Polyaxial screws have been subsequently implemented and designed to provide increased freedom on the screw-to-rod connection to

facilitate easier rod seating into the screw head saddle. It has been shown that adjacent segment degeneration is less likely to be observed in polyaxial pedicle screw fixation than in monoaxial fixation due to lower von Mises stress in the polyaxial pedicle screws compared to the monoaxial pedicle screws.  $^{61}$  A compromise between monoaxial and polyaxial screws was the uniplanar or uniaxial screw construct, designed to accommodate sagittal angle variation of the pedicle screws with respect to rods. Uniplanar screws showed less residual apical vertebral rotation after a 1-year postoperative evaluation (p < 0.001).  $^{62}$ 

Problems associated with pedicle screws include loss of fixation, improper placement, fatigue and bending failure, dural tears, cerebral spinal fluid leaks, nerve root injury, and infection. <sup>63-65</sup> Bending or breakage is the most common type of pedicle screw failure. <sup>66</sup> Screw diameter, screw length, insertional depth, orientation, and cross-link conduits all affect bending and breakage. <sup>67</sup> Biomechanical studies show that osteoporosis, cortical fixation, pedicle morphology, screw orientation, bone density, screw thread area, and screw orientation all affect pedicle screw pullout. <sup>68,69</sup>

#### 4. Plates

Spinal plates are a pinnacle implant to stabilize and restore normal alignment to the spine. Biomechanical experiments for stress-strain analyses performed from T12-L4 and suggested that a titanium-plate fixation and laminectomy was more stable than just laminectomy or just a plate (p < 0.05). Many plates are traditionally made of PTi or Ti6Al4V.71 Some plates have been developed to incorporate additional elements such as polyethylene ring utilized as a screw locking mechanism within the plate.<sup>72</sup> New developments in spinal plate technology include development of biodegradable plates that have been developed and tested in vitro compared to the standard titanium plate. The strong biodegradable plate and bone block (PLA-4G) have similar range of motion, torque strength, and von Mises stress results as titanium, and has a lower Young's modulus compared to titanium (4,000 N/mm<sup>2</sup> vs. 10,000 N/mm<sup>2</sup>).<sup>73</sup> The biodegradable plate is not paramagnetic, reducing artifacts on future imaging studies.

Mini-plate systems are extensively applied to cervical laminoplasty for patients with multilevel cervical compressive myelopathy and to secure the posterior elements in the open position after an expansive open-door laminoplasty.<sup>74</sup> These miniplates are typically made of titanium, but research into developing a cheaper model for mini-plates is ongoing.<sup>75</sup>

#### **NEW DEVELOPMENTS**

#### 1. Lumbar Spine Disc Replacement

Total disc replacement (TDR) has yielded comparable or superior outcomes compared to lumbar fusion over a 2-year time period, preserving functional movement unlike with spinal fusion.76 TDR had a relatively low rate of complications after a 5-year meta-analysis for lumbar TDR (0%-16.7%) and cervical (0%-4.0%).<sup>77</sup> The first lumbar disc replacement was a steel ball implanted in 1960, which ultimately led to multiple postoperative complications.<sup>78</sup> In the 1980s, the implants shifted from a SS ball to 2 plates made of steel or titanium with a polyethylene sliding core in between them.<sup>79</sup> There was an additional implant called the SB Chartie prothesis which consisted of 2 chromium-cobalt plates and a mobile polyethylene core.80 In 1989, the ProDisk-L was developed which had plates with a central titanium stem.<sup>81</sup> Ceramics were considered since they are more resistant to wear, but are significantly more fragile due to their low ductility. Surface coatings and anchorage to promote osseointegration ranged from HA, tricalcium phosphate, porous titanium or chromium-cobalt.

The ProDisc-L implants are made of a cobalt-chromium-molybdenum with an ultra-high molecular weight polyethylene combined with a rough titanium surface coating to promote bone growth alloy.  $^{82}$  ProDisc-L showed significant improvement in fusion and Oswestry Disability Index (p < 0.001) compared to circumferential arthrodesis.  $^{82}$ 

The ApiFix system is a new, less-invasive fusionless scoliosis correction system that connects 2 periapical pedicle screws through polyaxial mobile ball-and-socket joints with a rod.<sup>83</sup> It was demonstrated that this implant halved the range of motion of flexion-extension (-40% in humans), Lateral bending was partially affected (-18.2% in humans), axial rotation was not affected.

#### 2. Cervical Spine Disc Replacement

The ProDisc-C implants are made of a cobalt-chromium-molybdenum with an ultra-high molecular weight polyethylene combined with a rough titanium surface coating to promote bone growth alloy. ProDisc-C has been found to restore range of motion of the entire neck back to preoperative state in late phase postoperative surgery. It was also suggested that segmental degenerative kyphosisc was significantly corrected in those who underwent ProDisc-C replacement. ProDisc-C replacement.

Another recent development is the Mobi-C cervical disc prothesis. The Mobi-C disc has 3 parts: 2 metal plates (typically made

out of cobalt, chromium and molybdenum) covered with a HA coating (to improve bone grafting) and a plastic plate (made from polyethylene) at the center. Mobi-C has demonstrated equal or increased improvement in range of motion, pain and short-form scores compared to the standard ACDE. It has been shown that Mobi-C artificial discs resulted in an improved neck disability index score, patient satisfaction and reduced surgical intervention compared to ACDE. Additional conclusive long-term clinical data is needed.

## THREE-DIMENSIONAL PRINTING, AND ADVANCES IN SPINAL IMPLANTS

Three-dimensional (3D) printing is the most frequently utilized in preoperative planning stages, printing templates out of plastic-including but not limited to acrylonitrile butadiene styrene, acrylate resin, acrylate resin, polyamide photosensitive resin, titanium, and polylactic acid.87 Pedicle screw templates have been printed with a 94.60% acceptable rate with cervical spine surgery.88 These models have been proven to reduce the perioperative blood loss during complicated spinal fusion surgeries as well as reduction in fluoroscopy time, improved communication with the surgical team, and lower rates of screw misplacements.<sup>89</sup> Models have also shown to reduce operation time by 15%-20% through a more involved pathology (location and surgical approach) as well as facilitation of preoperative instrumentation decisions.89 These models cost an additional \$300 to over \$1,000 and take between 5 hours and 2 days to create.90 However, limitations with preoperative modeling exist ranging from lack of surgically useful information such as joint instability and a sense of real-time information as provided with imaging combined with a significant learning curve for the software and hardware required to create the models. 87,88,91

Arguably the most exciting application of 3D printing is the ability of surgeons to create specifically-designed implants for each patient. So far, a majority of the implants have been made out of titanium (TiV6Al4) due to its biocompatibility for applications ranging from C1/2 posterior fixation devices to Sacrum replacements. 92-94 However, there is an increased research effort towards 3D printing biodegradable scaffolds using a degradable polyurethane to mimic the elasticity of the intervertebral disc. 95 Tissue and bone engineering is being explored as possible alternatives to biodegradable plastics for intervertebral discs and other spinal implants. 96

#### **CONCLUSION**

Spinal implants have come a long way from the original 1890s silver wire fusion methods. Now, the standard material is either PEEK or titanium. New research is being conducted to find materials with increased bone grafting properties (by doping existing materials or developing new materials), improving strength/Young's modulus, and developing novel ideas to prevent further postoperative complications by improving range of motion, decreasing pain, distributing anatomic forces to decrease adjacent segment disease, and minimizing the necessity for additional spinal surgery. New developments in biomaterials for spinal implants and the advent of new technologies, like 3D printed patient-specific implants, have made incredible progress in biocompatibility of spinal tools. Spine surgeons should remain vigilant regarding the current literature and technological advancements in spinal materials and procedures.

#### **CONFLICT OF INTEREST**

The authors have nothing to disclose.

#### REFERENCES

- Tarpada SP, Morris MT, Burton DA. Spinal fusion surgery: a historical perspective. J Orthop 2017;14:134-6.
- Hadra BE. The classic: wiring of the vertebrae as a means of immobilization in fracture and Potts' disease. Berthold E. Hadra. Med Times and Register, Vol22, May 23, 1891. Clin Orthop Relat Res 1975;(112):4-8.
- Bohlman HH. Acute fractures and dislocations of the cervical spine. An analysis of three hundred hospitalized patients and review of the literature. J Bone Joint Surg Am 1979;61: 1119-42.
- Cahill DW, Bellegarrigue R, Ducker TB. Bilateral facet to spinous process fusion: a new technique for posterior spinal fusion after trauma. Neurosurgery 1983;13:1-4.
- Callahan RA, Johnson RM, Margolis RN, et al. Cervical facet fusion for control of instability following laminectomy. J Bone Joint Surg Am 1977;59:991-1002.
- Yoshihara H. Rods in spinal surgery: a review of the literature. Spine J 2013;13:1350-8.
- 7. Merriwether M, Shockey, R, inventors; Box cage for intervertebral body fusion. United States patent. US1,9990,436,593.1999, November 09.
- 8. Kersten RF, van Gaalen SM, de Gast A, et al. Polyetherether-

- ketone (PEEK) cages in cervical applications: a systematic review. Spine J 2015;15:1446-60.
- Farrokhi MR, Nikoo Z, Gholami M, et al. Comparison between acrylic cage and polyetheretherketone (PEEK) cage in single-level anterior cervical discectomy and fusion: a randomized clinical trial. Clin Spine Surg 2017;30:38-46.
- 10. Kienle A, Graf N, Wilke HJ. Does impaction of titanium-coated interbody fusion cages into the disc space cause wear debris or delamination? Spine J 2016;16:235-42.
- 11. Suh PB, Puttlitz C, Lewis C, et al. The effect of cervical interbody cage morphology, material composition, and substrate density on cage subsidence. J Am Acad Orthop Surg 2017;25:160-8.
- 12. Kersten RF, van Gaalen SM, Arts MP, et al. The SNAP trial: a double blind multi-center randomized controlled trial of a silicon nitride versus a PEEK cage in transforaminal lumbar interbody fusion in patients with symptomatic degenerative lumbar disc disorders: study protocol. BMC Musculoskelet Disord 2014;15:57.
- Richardson B, Paulzak A, Rusyniak WG, et al. Anterior lumbar corpectomy with expandable titanium cage reconstruction: a case series of 42 patients. World Neurosurg 2017;108: 317-24.
- 14. Seaman S, Kerezoudis P, Bydon M, et al. Titanium vs. polyetheretherketone (PEEK) interbody fusion: meta-analysis and review of the literature. J Clin Neurosci 2017;44:23-9.
- 15. Datla NV, Konh B, Koo JJ, et al. Polyacrylamide phantom for self-actuating needle-tissue interaction studies. Med Eng Phys 2014;36:140-5.
- 16. McGilvray KC, Easley J, Seim HB, et al. Bony ingrowth potential of 3D-printed porous titanium alloy: a direct comparison of interbody cage materials in an in vivo ovine lumbar fusion model. Spine J 2018;18:1250-60.
- 17. Majd ME, Vadhva M, Holt RT. Anterior cervical reconstruction using titanium cages with anterior plating. Spine (Phila Pa 1976) 1999;24:1604-10.
- Long M, Rack HJ. Titanium alloys in total joint replacementa materials science perspective. Biomaterials 1998;19:1621-39
- 19. Kong F, Nie Z, Liu Z, et al. Developments of nano-TiO2 incorporated hydroxyapatite/PEEK composite strut for cervical reconstruction and interbody fusion after corpectomy with anterior plate fixation. J Photochem Photobiol B 2018; 187:120-5.
- 20. Kuo MC, Tsai CM, Huang JC, et al. PEEK composites reinforced by nano-sized SiO2 and A12O3^Os particulates. Ma-

- ter Chem Phys 2005;90:185-95.
- 21. Jiang N, Huang J, Edwards LJ, et al. Two-stage cooperative T cell receptor-peptide major histocompatibility complex-CD8 trimolecular interactions amplify antigen discrimination. Immunity 2011;34:13-23.
- 22. Vadapalli S, Sairyo K, Goel VK, et al. Biomechanical rationale for using polyetheretherketone (PEEK) spacers for lumbar interbody fusion-A finite element study. Spine (Phila Pa 1976) 2006;31:E992-8.
- 23. Chen Y, Wang X, Lu X, et al. Comparison of titanium and polyetheretherketone (PEEK) cages in the surgical treatment of multilevel cervical spondylotic myelopathy: a prospective, randomized, control study with over 7-year follow-up. Eur Spine J 2013;22:1539-46.
- 24. Kersten R, Wu G, Pouran B, et al. Comparison of polyetheretherketone versus silicon nitride intervertebral spinal spacers in a caprine model. J Biomed Mater Res B Appl Biomater 2019;107:688-99.
- 25. Natarajan RN, Watanabe K, Hasegawa K. Biomechanical analysis of a long-segment fusion in a lumbar spine-a finite element model study. J Biomech Eng 2018;140(9). https://doi.org/10.1115/1.4039989.
- 26. Kang H, Hollister SJ, La Marca F, et al. Porous biodegradable lumbar interbody fusion cage design and fabrication using integrated global-local topology optimization with laser sintering. J Biomech Eng 2013;135:101013-8.
- 27. Harrington PR. Treatment of scoliosis. Correction and internal fixation by spine instrumentation. J Bone Joint Surg Am 1962;44-A:591-610.
- 28. Lindsey C, Deviren V, Xu Z, et al. The effects of rod contouring on spinal construct fatigue strength. Spine (Phila Pa 1976) 2006;31:1680-7.
- 29. Glotzbecker MP, Riedel MD, Vitale MG, et al. What's the evidence? Systematic literature review of risk factors and preventive strategies for surgical site infection following pediatric spine surgery. J Pediatr Orthop 2013;33:479-87.
- 30. Asher MA, Carson WL, Hardacker JW, et al. The effect of arthrodesis, implant stiffness, and time on the canine lumbar spine. J Spinal Disord Tech 2007;20:549-59.
- 31. Dobbs MB, Lenke LG, Kim YJ, et al. Anterior/posterior spinal instrumentation versus posterior instrumentation alone for the treatment of adolescent idiopathic scoliotic curves more than 90 degrees. Spine (Phila Pa 1976) 2006;31:2386-91.
- 32. Gotman I. Characteristics of metals used in implants. J Endourol 1997;6:383-9.

- 33. Ebraheim NA, Rupp RE, Savolaine ER, et al. Posterior plating of the cervical spine. J Spinal Disord 1995;8:111-5.
- 34. Serhan H, Mhatre D, Newton P, et al. Would CoCr rods provide better correctional forces than stainless steel or titanium for rigid scoliosis curves? J Spinal Disord Tech 2013;26: E70-74.
- 35. Angelliaume A, Ferrero E, Mazda K, et al. Titanium vs cobalt chromium: what is the best rod material to enhance adolescent idiopathic scoliosis correction with sublaminar bands? Eur Spine J 2017;26:1732-8.
- 36. Ahmad FU, Sidani C, Fourzali R, et al. Postoperative magnetic resonance imaging artifact with cobalt-chromium versus titanium spinal instrumentation: presented at the 2013 Joint Spine Section Meeting. Clinical article. J Neurosurg Spine 2013;19:629-36.
- 37. Buehler WJ, Wang FE. A summary of recent research on the nitinol alloys and their potential application in ocean engineering. Ocean Eng 1968;1:105-20.
- 38. Rhalmi S, Charette S, Assad M, et al. The spinal cord dura mater reaction to nitinol and titanium alloy particles: a 1-year study in rabbits. Eur Spine J 2007;16:1063-72.
- 39. Biesiekierski A, Wang J, Gepreel MA, et al. A new look at biomedical Ti-based shape memory alloys. Acta Biomater 2012;8:1661-9.
- 40. Ponnappan RK, Serhan H, Zarda B, et al. Biomechanical evaluation and comparison of polyetheretherketone rod system to traditional titanium rod fixation. Spine J 2009;9:263-7.
- 41. Cook SD, Patron LP, Christakis PM, et al. Comparison of methods for determining the presence and extent of anterior lumbar interbody fusion. Spine (Phila Pa 1976) 2004;29: 1118-23.
- 42. Grob D, Benini A, Junge A, et al. Clinical experience with the Dynesys semirigid fixation system for the lumbar spine: surgical and patient-oriented outcome in 50 cases after an average of 2 years. Spine (Phila Pa 1976) 2005;30:324-31.
- 43. Dick JC, Bourgeault CA. Notch sensitivity of titanium alloy, commercially pure titanium, and stainless steel spinal implants. Spine (Phila Pa 1976) 2001;26:1668-72.
- 44. Zhao X, Niinomi M, Nakai M, et al. Beta type Ti-Mo alloys with changeable Young's modulus for spinal fixation applications. Acta Biomater 2012;8:1990-7.
- 45. Nguyen TQ, Buckley JM, Ames C, et al. The fatigue life of contoured cobalt chrome posterior spinal fusion rods. Proc Inst Mech Eng H 2011;225:194-8.
- 46. Liu H, Niinomi M, Nakai M, et al. Mechanical properties and cytocompatibility of oxygen-modified beta-type Ti-Cr

- alloys for spinal fixation devices. Acta Biomater 2015;12:352-61.
- 47. Jacobs E, Roth AK, Arts JJ, et al. Reduction of intradiscal pressure by the use of polycarbonate-urethane rods as compared to titanium rods in posterior thoracolumbar spinal fixation. J Mater Sci Mater Med 2017;28:148. https://doi.org/10.1007/s10856-017-5953-0.
- 48. Tsuang FY, Hsieh YY, Kuo YJ, et al. Assessment of the suitability of biodegradable rods for use in posterior lumbar fusion: an in-vitro biomechanical evaluation and finite element analysis. PLoS One 2017;12:e0188034.
- 49. Lee SM, Suk SI, Chung ER. Direct vertebral rotation: a new technique of three-dimensional deformity correction with segmental pedicle screw fixation in adolescent idiopathic scoliosis. Spine (Phila Pa 1976) 2004;29:343-9.
- 50. Liu B, Liu R, Wang L. A meta-analysis of the preoperative use of gabapentinoids for the treatment of acute postoperative pain following spinal surgery. Medicine (Baltimore) 2017; 96:e8031.
- 51. Jansen JA, van de Waerden JP, Wolke JG, et al. Histologic evaluation of the osseous adaptation to titanium and hydroxyapatite-coated titanium implants. J Biomed Mater Res 1991;25:973-89.
- 52. Hasegawa T, Inufusa A, Imai Y, et al. Hydroxyapatite-coating of pedicle screws improves resistance against pull-out force in the osteoporotic canine lumbar spine model: a pilot study. Spine J 2005;5:239-43.
- 53. Sanden B, Olerud C, Johansson C, et al. Improved bone-screw interface with hydroxyapatite coating: an in vivo study of loaded pedicle screws in sheep. Spine (Phila Pa 1976) 2001; 26:2673-8.
- 54. Yi S, Rim DC, Park SW, et al. Biomechanical comparisons of pull out strengths after pedicle screw augmentation with hydroxyapatite, calcium phosphate, or polymethylmethacrylate in the cadaveric spine. World Neurosurg 2015;83:976-81.
- 55. Shi LY, Wang A, Zang FZ, et al. Tantalum-coated pedicle screws enhance implant integration. Colloids Surf B Biointerfaces 2017;160:22-32.
- 56. Liu GM, Kong N, Zhang XY, et al. Extracellular matrix-coating pedicle screws conduct and induce osteogenesis. Eur J Orthop Surg Traumatol 2014;24 Suppl 1:S173-82.
- 57. Lotz JC, Hu SS, Chiu DF, et al. Carbonated apatite cement augmentation of pedicle screw fixation in the lumbar spine. Spine (Phila Pa 1976) 1997;22:2716-23.
- 58. Lonner BS, Auerbach JD, Boachie-Adjei O, et al. Treatment

- of thoracic scoliosis: are monoaxial thoracic pedicle screws the best form of fixation for correction? Spine (Phila Pa 1976) 2009;34:845-51.
- 59. Vigneswaran HT, Grabel ZJ, Eberson CP, et al. Surgical treatment of adolescent idiopathic scoliosis in the United States from 1997 to 2012: an analysis of 20,346 patients. J Neurosurg Pediatr 2015;16:322-8.
- 60. Duncan JW, Bailey RA. An analysis of fusion cage migration in unilateral and bilateral fixation with transforaminal lumbar interbody fusion. Eur Spine J 2013;22:439-45.
- 61. Wang H, Zhao Y, Mo Z, et al. Comparison of short-segment monoaxial and polyaxial pedicle screw fixation combined with intermediate screws in traumatic thoracolumbar fractures: a finite element study and clinical radiographic review. Clinics (Sao Paulo) 2017;72:609-17.
- 62. Dalal A, Upasani VV, Bastrom TP, et al. Apical vertebral rotation in adolescent idiopathic scoliosis: comparison of uniplanar and polyaxial pedicle screws. J Spinal Disord Tech 2011;24:251-7.
- 63. Esses SI, Sachs BL, Dreyzin V. Complications associated with the technique of pedicle screw fixation. A selected survey of ABS members. Spine (Phila Pa 1976) 1993;18:2231-8, discussion 2238-9.
- 64. Ransom N, La Rocca SH, Thalgott J. The case for pedicle fixation of the lumbar spine. Spine (Phila Pa 1976) 1994;19: 2702-6.
- 65. Weinstein JN, Spratt KF, Spengler D, et al. Spinal pedicle fixation: reliability and validity of roentgenogram-based assessment and surgical factors on successful screw placement. Spine (Phila Pa 1976) 1988;13:1012-8.
- 66. Pfeiffer M, Hoffman H, Goel VK, et al. In vitro testing of a new transpedicular stabilization technique. Eur Spine J 1997; 6:249-55.
- 67. McKinley TO, McLain RF, Yerby SA, et al. The effect of pedicle morphometry on pedicle screw loading. A synthetic model. Spine (Phila Pa 1976) 1997;22:246-52.
- 68. Pfeiffer M, Gilbertson LG, Goel VK, et al. Effect of specimen fixation method on pullout tests of pedicle screws. Spine (Phila Pa 1976) 1996;21:1037-44.
- 69. Soshi S, Shiba R, Kondo H, et al. An experimental study on transpedicular screw fixation in relation to osteoporosis of the lumbar spine. Spine (Phila Pa 1976) 1991;16:1335-41.
- 70. Nong L, Zhou D, Xu N, et al. Lamina replacement with titanium plate fixation improves spinal stability after total lumbar laminectomy. Comput Methods Biomech Biomed Engin 2015;18:1753-9.

- 71. Kamaljit, P, inventors; Medtronic, assignee. Spinal plate assembly. United States patent US 8221476B2. 2003, July 24.
- 72. Lao L, Li Q, Zhong G, et al. Biomechanical study of a novel self-locking plate system for anterior cervical fixation. J Orthop Surg Res 2014;9:120.
- 73. Cho PG, Ji GY, Park SH, et al. Biomechanical analysis of biodegradable cervical plates developed for anterior cervical discectomy and fusion. Asian Spine J 2018;12:1092-9.
- 74. Suda K, Abumi K, Ito M, et al. Local kyphosis reduces surgical outcomes of expansive open-door laminoplasty for cervical spondylotic myelopathy. Spine (Phila Pa 1976) 2003;28: 1258-62.
- 75. Hu W, Shen X, Sun T, et al. Laminar reclosure after single open-door laminoplasty using titanium miniplates versus suture anchors. Orthopedics 2014;37:e71-8.
- 76. Jacobs WC, van der Gaag NA, Kruyt MC, et al. Total disc replacement for chronic discogenic low back pain: a Cochrane review. Spine (Phila Pa 1976) 2013;38:24-36.
- 77. Formica M, Divano S, Cavagnaro L, et al. Lumbar total disc arthroplasty: outdated surgery or here to stay procedure? A systematic review of current literature. J Orthop Traumatol 2017;18:197-215.
- 78. Fernstrom U. Arthroplasty with intercorporal endoprothesis in herniated disc and in painful disc. Acta Chir Scand Suppl 1966;357:154-9.
- 79. Buttner-Janz K, Schellnack K, Zippel H. An alternative treatment strategy in lumbar intervertebral disk damage using an SB Charite modular type intervertebral disk endoprosthesis. Z Orthop Ihre Grenzgeb 1987;125:1-6.
- 80. Blondel B, Tropiano P, Gaudart J, et al. Clinical results of lumbar total disc arthroplasty in accordance with Modic signs, with a 2-year-minimum follow-up. Spine (Phila Pa 1976) 2011;36:2309-15.
- 81. Vital JM, Boissiere L. Total disc replacement. Orthop Traumatol Surg Res 2014;100(1 Suppl):S1-14.
- 82. Zigler JE, Delamarter R, Murrey D, et al. ProDisc-C and anterior cervical discectomy and fusion as surgical treatment for single-level cervical symptomatic degenerative disc disease: five-year results of a Food and Drug Administration study. Spine (Phila Pa 1976) 2013;38:203-9.
- 83. Holewijn RM, de Kleuver M, van der Veen AJ, et al. A novel spinal implant for fusionless scoliosis correction: a biomechanical analysis of the motion preserving properties of a posterior periapical concave distraction device. Global Spine J 2017;7:400-9.
- 84. Ahn PG, Kim KN, Moon SW, et al. Changes in cervical range

- of motion and sagittal alignment in early and late phases after total disc replacement: radiographic follow-up exceeding 2 years. J Neurosurg Spine 2009;11:688-95.
- 85. Lu H, Peng L. Efficacy and safety of Mobi-C cervical artificial disc versus anterior discectomy and fusion in patients with symptomatic degenerative disc disease: a meta-analysis. Medicine (Baltimore) 2017;96:e8504.
- 86. Alvin MD, Mroz TE. The Mobi-C cervical disc for one-level and two-level cervical disc replacement: a review of the literature. Med Devices (Auckl) 2014;7:397-403.
- 87. Mao K, Wang Y, Xiao S, et al. Clinical application of computer-designed polystyrene models in complex severe spinal deformities: a pilot study. Eur Spine J 2010;19:797-802.
- 88. Guo F, Dai J, Zhang J, et al. Individualized 3D printing navigation template for pedicle screw fixation in upper cervical spine. PLoS One 2017;12:e0171509.
- 89. Izatt MT, Thorpe PL, Thompson RG, et al. The use of physical biomodelling in complex spinal surgery. Eur Spine J 2007; 16:1507-18.
- 90. Wu ZX, Huang LY, Sang HX, et al. Accuracy and safety assessment of pedicle screw placement using the rapid prototyping technique in severe congenital scoliosis. J Spinal Disord Tech 2011;24:444-50.
- 91. Li C, Yang M, Xie Y, et al. Application of the polystyrene model made by 3-D printing rapid prototyping technology for operation planning in revision lumbar discectomy. J Orthop Sci 2015;20:475-80.
- 92. Xu N, Wei F, Liu X, et al. Reconstruction of the upper cervical spine using a personalized 3D-printed vertebral body in an adolescent with ewing sarcoma. Spine (Phila Pa 1976) 2016;41:E50-4.
- 93. Kim D, Lim JY, Shim KW, et al. Sacral reconstruction with a 3D-printed implant after hemisacrectomy in a patient with sacral osteosarcoma: 1-year follow-up result. Yonsei Med J 2017;58:453-7.
- 94. Mobbs, RJ, Coughlan, M, Thompson, R, et al. The utility of 3D printing for surgical planning and patient-specific implant design for complex spinal pathologies: case report. J Neurosurg Spine 2017;26:513-8.
- 95. Whatley BR, Kuo J, Shuai C, et al. Fabrication of a biomimetic elastic intervertebral disk scaffold using additive manufacturing. Biofabrication 2011;3:015004.
- 96. Ursan ID, Chiu L, Pierce A. Three-dimensional drug printing: a structured review. J Am Pharm Assoc (2003) 2013;53: 136-44.